Constitutive Relations, Natural States, and Travelling Waves in Two-Dimensional Nonlinear Elastodynamics

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- Governing Equations for Hyperelastic Materials
- Constitutive Relations

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- Details of the Model
- Reduction of Number of Parameters

3 C-M-R Elasticity Equations in 2D

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- Symmetries of Differential Equations
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- Traveling Wave Coordinates
- Examples of Exact Solutions

Conclusions and Open Problems

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J.-F. Ganghoffer, LEMTA - ENSEM, Université de Lorraine, Nancy, France

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Notation

Notation

•
$$\frac{\partial u}{\partial x} \equiv u_x$$

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Fig. 1. Material and Eulerian coordinates.

Material picture

- A solid body occupies the reference (Lagrangian) volume $\Omega_0 \subset \mathbb{R}^3$.
- Actual (Eulerian) configuration: $\Omega \subset \mathbb{R}^3$.
- Material points are labelled by $\mathbf{X} \in \Omega_0$.
- The actual position of a material point: $\mathbf{x} = \phi(\mathbf{X}, t) \in \Omega$.



Fig. 1. Material and Eulerian coordinates.

Material picture

- Velocity of a material point X: $\mathbf{v}(\mathbf{X}, t) = \frac{d\mathbf{x}}{dt}$.
- Jacobian matrix (deformation gradient):

$$\mathbf{F}(\mathbf{X}, t) = \nabla \phi; \quad J = \det \mathbf{F} > 0;$$
$$\mathbf{F} = \{F_{ii}\} = \{F_{ii}^{i}\}.$$



Fig. 1. Material and Eulerian coordinates.

Material picture

- Boundary force (per unit area) in Eulerian configuration: $\mathbf{t} = \boldsymbol{\sigma} \mathbf{n}$.
- Boundary force (per unit area) in Lagrangian configuration: **T** = **PN**.
- $\sigma = \sigma(\mathbf{x}, t)$ is the Cauchy stress tensor.
- $\mathbf{P} = J\boldsymbol{\sigma}\mathbf{F}^{-T}$ is the first Piola-Kirchhoff tensor.

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Fig. 1. Material and Eulerian coordinates.

Material picture

- Density in reference configuration: $\rho_0 = \rho_0(\mathbf{X})$ (time-independent).
- Density in actual configuration:

$$\rho = \rho(\mathbf{X}, t) = \rho_0/J.$$

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Equations of motion (no dissipation, purely elastic setting):

$$\rho_0 \mathbf{x}_{tt} = \mathsf{div}_{(X)} \mathbf{P} + \rho_0 \mathbf{R},\tag{1}$$

• $\mathbf{R} = \mathbf{R}(\mathbf{X}, t)$: total body force per unit mass.

• $(\operatorname{div}_{(X)}\mathbf{P})^i = \frac{\partial P^{ij}}{\partial X^j}.$

Cauchy stress tensor symmetry (conservation of angular momentum):

$$\mathbf{F}\mathbf{P}^{\mathsf{T}} = \mathbf{P}\mathbf{F}^{\mathsf{T}} \quad \Leftrightarrow \quad \boldsymbol{\sigma} = \boldsymbol{\sigma}^{\mathsf{T}}.$$
 (2)

The first Piola-Kirchhoff stress tensor:

$$\mathbf{P} =
ho_0 rac{\partial W}{\partial \mathbf{F}}, \qquad P^{ij} =
ho_0 rac{\partial W}{\partial F_{ij}}.$$

• $W = W(\mathbf{X}, \mathbf{F})$: a scalar strain energy density function.

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Isotropic Homogeneous Hyperelastic Materials

• Strain energy density W depends only on certain matrix invariants:

$$W=U(I_1,I_2,I_3).$$

• For the left Cauchy-Green strain tensor $\mathbf{B} = \mathbf{F}\mathbf{F}^{\mathsf{T}}$,

 $I_{1} = \operatorname{Tr} \mathbf{B} = F_{k}^{i} F_{k}^{i},$ $I_{2} = \frac{1}{2} [(\operatorname{Tr} \mathbf{B})^{2} - \operatorname{Tr}(\mathbf{B}^{2})] = \frac{1}{2} (I_{1}^{2} - B^{ik} B^{ki}),$ $I_{3} = \det \mathbf{B} = J^{2}.$

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Isotropic Homogeneous Hyperelastic Materials

• Strain energy density W depends only on certain matrix invariants:

 $W = U(I_1, I_2, I_3).$

Table 1: Neo-Hookean and Mooney-Rivlin constitutive models

Туре	Neo-Hookean	Mooney-Rivlin
Standard	$W = al_1,$	$W=al_1+bl_2,$
	<i>a</i> > 0.	a, b > 0
Generalized	$W = a\overline{l}_1 + c(J-1)^2,$	$W=aar{l}_1+bar{l}_2+c(J-1)^2$
	a, c > 0.	a, b, c > 0
Generalized (Ciarlet)	$W = aI_1 + \Gamma(J),$	$W = aI_1 + bI_2 + \Gamma(J)$
"compressible"	$\Gamma(q) = cq^2 - d\log q, a, c, d > 0$	$\Gamma(q) = cq^2 - d\log q, a, b, c, d > 0$

Isotropic Homogeneous Hyperelastic Materials

• Strain energy density W depends only on certain matrix invariants:

 $W = U(I_1, I_2, I_3).$

Example: the Neo-Hookean Case

- Strain energy density: $W = a I_1$, a = const.
- Equations of motion are linear and decoupled:

$$(x^{k})_{tt} = a \left(\frac{\partial^2}{\partial (X^1)^2} + \frac{\partial^2}{\partial (X^2)^2} + \frac{\partial^2}{\partial (X^3)^2} \right) x^{k},$$

k = 1, 2, 3.

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Ciarlet-Mooney-Rivlin solids in 2D: Governing equations

General equations:

$$\begin{split} \rho_0 \mathbf{x}_{tt} &= \mathsf{div}_{(X)} \mathbf{P} + \rho_0 \mathbf{R}, \\ \mathbf{F} \mathbf{P}^T &= \mathbf{P} \mathbf{F}^T, \\ \mathbf{P} &= \rho_0 \; \partial W / \partial \mathbf{F}. \end{split}$$

Assumptions:

- Two-dimensional: $x^{1,2} = x^{1,2}(X^1, X^2, t)$; the third coordinate $x^3 = X^3$ is fixed.
- Ciarlet-Mooney-Rivlin constitutive relation (4 parameters):

$$W = aI_1 + bI_2 - cI_3 - \frac{1}{2}d\log I_3, \quad a > 0, \quad b, c, d \ge 0,$$
(4)

$$\mathbf{F} = \begin{bmatrix} F_{11} & F_{12} & 0\\ F_{21} & F_{22} & 0\\ 0 & 0 & 1 \end{bmatrix}, \qquad \begin{array}{c} \rho_0(x^1)_{tt} - \frac{\partial P^{11}}{\partial X^1} - \frac{\partial P^{12}}{\partial X^2} - \rho_0 R^1 = 0, \\ \rho_0(x^2)_{tt} - \frac{\partial P^{21}}{\partial X^1} - \frac{\partial P^{22}}{\partial X^2} - \rho_0 R^2 = 0. \end{array}$$

Ciarlet-Mooney-Rivlin constitutive relation:

$$W=aI_1+bI_2-cI_3-rac{1}{2}d\log I_3,\quad a>0,\quad b,c,d\geq 0.$$

Equivalence Transformations:

$$\begin{split} \widetilde{t} &= e^{\varepsilon_2} t + \varepsilon_1, \qquad \widetilde{x}^1 = e^{2\varepsilon_2} x^1, \qquad \widetilde{x}^2 = e^{2\varepsilon_2} x^2, \\ \widetilde{X}^1 &= e^{\varepsilon_3} \left(X^1 \cos \varepsilon_7 - X^2 \sin \varepsilon_7 \right) + \varepsilon_4, \qquad \widetilde{X}^2 = e^{\varepsilon_3} \left(X^1 \sin \varepsilon_7 + X^2 \sin \varepsilon_7 \right) + \varepsilon_5, \\ \widetilde{\rho_0} &= e^{\varepsilon_6} \rho_0, \qquad \widetilde{R}^1 = R^1, \qquad \widetilde{R}^2 = R^2, \\ \widetilde{a} &= -b + e^{2\varepsilon_3 - 2\varepsilon_2} (a + b), \qquad \widetilde{b} = b, \qquad \widetilde{c} = -b + e^{4\varepsilon_3 - 6\varepsilon_2} (b + c), \qquad \widetilde{d} = e^{2\varepsilon_2} d. \end{split}$$

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Ciarlet-Mooney-Rivlin constitutive relation:

$$W = aI_1 + bI_2 - cI_3 - \frac{1}{2}d\log I_3, \quad a > 0, \quad b, c, d \ge 0.$$

Principal Result 1:

• The model essentially depends on three constitutive parameters:

$$A = 2(a+b) \ge 0$$
, $B = 2(b+c) \ge 0$, d .

• the two-dimensional first Piola-Kirchhoff stress tensor is given by

$$\mathbf{P}_2 = \rho_0 \left[\mathbf{A} \, \mathbf{F}_2 + \mathbf{B} \, J \, \mathbf{C}_2 - \frac{d}{J} \, \mathbf{C}_2 \right],$$

where

$$\mathbf{F_2} = \begin{bmatrix} F_1^1 & F_1^2 \\ F_1^2 & F_2^2 \end{bmatrix}, \quad \mathbf{C_2} = \begin{bmatrix} F_2^2 & -F_1^2 \\ -F_1^2 & F_1^1 \end{bmatrix},$$

$$\mathbf{F}_2 = \nabla_{(X)} \mathbf{x}, \quad \mathbf{x} = [x^1(\mathbf{X}, t), x^2(\mathbf{X}, t)]^T.$$

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Governing equations:

- No forcing: $R^1 = R^2 = 0$.
- Dynamic equations:

$$\rho_0(x^1)_{tt} - \frac{\partial P^{11}}{\partial X^1} - \frac{\partial P^{12}}{\partial X^2} = 0,$$

$$\rho_0(x^2)_{tt} - \frac{\partial P^{21}}{\partial X^1} - \frac{\partial P^{22}}{\partial X^2} = 0.$$

• C-M-R constitutive relation:

$$\mathbf{P}_{2} = \rho_{0} \begin{bmatrix} \mathbf{A} \mathbf{F}_{2} + \mathbf{B} J \mathbf{C}_{2} - \frac{d}{J} \mathbf{C}_{2} \end{bmatrix},$$
$$\mathbf{F}_{2} = \begin{bmatrix} F_{1}^{1} & F_{2}^{1} \\ F_{1}^{2} & F_{2}^{2} \end{bmatrix}, \quad \mathbf{C}_{2} = \begin{bmatrix} F_{2}^{2} & -F_{1}^{2} \\ -F_{1}^{1} & F_{1}^{1} \end{bmatrix},$$
$$\mathbf{F}_{2} = \nabla_{(X)} \mathbf{x}, \quad \mathbf{x} = \begin{bmatrix} x^{1} (\mathbf{X}, t), x^{2} (\mathbf{X}, t) \end{bmatrix}^{T}.$$

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Specific Forms of Equations

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$$\begin{aligned} xI_{i,i} &= \frac{1}{\left(xI_{XI}xI_{22}^{2} - xI_{X2}xI_{XI}^{2}\right)^{2}} \left(xI_{XI,X2}^{2} xI_{X2}^{2}^{3} xI_{XI}^{3} B \\ &+ xI_{X2,X2}^{2} xI_{X2}^{2}^{2} xI_{21}^{4} B + xI_{XI,XI}^{2} xI_{X2}^{2} xI_{22}^{2} A \\ &+ xI_{X2,X2}^{2} xI_{X1}^{2} xI_{22}^{2} A + xI_{XI,XI}^{2} xI_{X2}^{2} xI_{X1}^{2} xI_{22}^{2} A \\ &+ xI_{X2,X2}^{2} xI_{X2}^{2} xI_{22}^{2} A + xI_{XI,XI}^{2} xI_{X2}^{2} xI_{X2}^{2} d + xI_{XI,XI}^{2} xI_{22}^{2} d \\ &- 2 xI_{XI,X2}^{2} xI_{22}^{2} d - xI_{22,X2}^{2} xI_{X1}^{3} xI_{22}^{2} xI_{22}^{2} d + xI_{XI,XI}^{2} xI_{22}^{2} d \\ &+ xI_{X2,X2}^{2} xI_{21}^{2} d - xI_{22,X2}^{2} xI_{11}^{3} xI_{22}^{2} xI_{21}^{2} d + xI_{XI,XI}^{2} xI_{22}^{2} d \\ &+ xI_{X2,X2}^{2} xI_{21}^{2} d - xI_{22,X2}^{2} xI_{11}^{3} xI_{22}^{2} xI_{21}^{3} B \\ &- x^{2} xI_{XI}^{2} xI_{21}^{2} xI_{22}^{2} xI_{21}^{2} B - 2 xI_{XI,X2}^{2} xI_{21}^{2} xI_{22}^{3} xI_{21}^{3} B \\ &+ xI_{X2,X2}^{2} xI_{12}^{2} xI_{22}^{2} xI_{21}^{2} B - 2 xI_{XI,X2}^{2} xI_{21}^{2} xI_{22}^{3} xI_{21}^{3} B \\ &+ xI_{X2,X2}^{2} xI_{12}^{2} xI_{22}^{2} xI_{21}^{2} B - 2 xI_{XI,X2}^{3} xI_{22}^{3} xI_{21}^{3} B \\ &+ xI_{X1,X1}^{3} xI_{22}^{2} xI_{22}^{2} xI_{21}^{2} B - 2 xI_{X1,X1}^{3} xI_{22}^{2} xI_{21}^{3} B \\ &+ xI_{X1,X1}^{3} xI_{22}^{2} xI_{22}^{2} xI_{21}^{2} B - 2 xI_{X1,X1}^{3} xI_{22}^{3} xI_{21}^{3} B \\ &+ xI_{X1,X1}^{3} xI_{22}^{2} xI_{22}^{2} xI_{22}^{2} xI_{22}^{3} xI_{22}^{3} xI_{22}^{3} B \\ &- 2 xI_{X1,X1}^{3} xI_{22}^{2} xI_{22}^{2} xI_{22}^{2} xI_{22}^{2} xI_{22}^{3} xI_{21}^{2} B \\ &- 2 xI_{X1,X2}^{3} xI_{22}^{3} xI_{22}^{2} xI_{22}^{3} B \\ &+ 2 x2_{2X2,X2}^{3} xI_{12}^{2} xZ_{21}^{3} xI_{22}^{2} xI_{21}^{2} B \\ &- 2 xI_{X1,X1}^{3} xI_{21}^{2} xI_{22}^{2} xI_{22}^{2} xI_{22}^{2} xI_{21}^{2} B \\ &- 2 xI_{X1,X1}^{3} xI_{21}^{2} xI_{22}^{2} xI_{22}^{2} xI_{21}^{2} B \\ &+ 2 xI_{2X1,X1}^{3} xI_{21}^{2} xI_{22}^{2} xI_{22}^{2} xI_{21}^{2} B \\ &+ 2 xI_{X1,X1}^{3} xI_{X1}^{3} xI_{22}^{2} xI_{22}^{3} xI_{21}^{3} B \\ &+ 2 xI_{X1,X2}^{3} xI_{X1}^{3} xI_{22}^{2} xI_{X2}^{3} B \\ &+ 2 xI_{X1,X2}^{3} xI_{X1}^{3} xI_{22}^{3} XI_{X2}^{3}$$

$$\begin{aligned} x 2_{t,t} &= \frac{1}{\left(x l_{X2} x 2_{X1}^2 - x l_{X1} x 2_{X2}\right)^2} \left(x 2_{X1, X1} x l_{X2}^2 d + x 2_{X2, X2} x l_{X1}^2 d \right. \\ &= 2 x 2_{X1, X1} x l_{X1} x 2_{X2} x l_{X2}^2 x 2_{X1} B = x l_{X1, X2} x l_{X1} x 2_{X2} x l_{X2}^2 x 2_{X1}^2 B \\ &+ 4 x 2_{X1, X2} x l_{X1}^2 x 2_{X2} x l_{X2}^2 x 2_{X1} B \\ &+ 2 x l_{X1, X1} x l_{X1} x 2_{X2}^2 x l_{X2}^2 x 2_{X1}^2 B \\ &+ 2 x l_{X2, X2} x l_{X1}^2 x 2_{X2} x l_{X2} x 2_{X1}^2 B \\ &- 2 x 2_{X1, X1} x l_{X1} x 2_{X2}^2 x l_{X2} x 2_{X1}^2 B \\ &- 2 x 2_{X2, X2} x l_{X1}^3 x 2_{X2} x l_{X2} x 2_{X1} B - x l_{X1, X2} x l_{X1}^2 x 2_{X2}^2 x l_{X2} x 2_{X1} B \\ &- 2 x 2_{X1, X1} x l_{X1} x 2_{X2} x l_{X2} x 2_{X1} B - x l_{X1, X2} x l_{X1}^2 x 2_{X2}^2 x l_{X2} x 2_{X1} B \\ &- 2 x 2_{X1, X1} x l_{X1} x 2_{X2} x l_{X2} x 2_{X1} A - 2 x 2_{X2, X2} x l_{X1} x l_{X2}^2 x 2_{X1} A \\ &+ x 2_{X1, X1} x l_{X1}^2 x 2_{X2}^2 x l_{X2}^2 B - 2 x 2_{X1, X2} x l_{X1} x l_{X2}^2 x 2_{X1}^2 B \\ &- x l_{X1, X1} x l_{X1}^2 x 2_{X2}^2 x l_{X2}^2 B - 2 x 2_{X1, X2} x l_{X1} x l_{X2}^2 x 2_{X1}^2 B \\ &- x l_{X1, X1} x l_{X1}^2 x 2_{X2}^2 x l_{X2}^2 B - 2 x 2_{X1, X2} x l_{X1} x l_{X2}^2 x 2_{X1}^2 B \\ &- x l_{X1, X1} x l_{X1}^2 x 2_{X2}^2 x l_{X2}^2 B - 2 x 2_{X1, X2} x l_{X1} x l_{X2}^2 x 2_{X1}^2 B \\ &- x l_{X1, X1} x l_{X1}^2 x 2_{X2}^2 x l_{X2}^2 B - 2 x 2_{X1, X2} x l_{X1}^3 x 2_{X2}^2 x l_{X2} B \\ &- x l_{X1, X1} x l_{X1}^2 x 2_{X2}^2 x l_{X2}^2 B - 2 x 2_{X1, X2} x l_{X1}^3 x 2_{X2}^2 x l_{X2} B \\ &- x l_{X1, X1} x l_{X1}^2 x 2_{X2}^3 x l_{X2} B - x l_{X2, X2} x l_{X1}^3 x 2_{X2}^2 x l_{X2} B \\ &- x l_{X1, X1} x l_{X1}^2 x 2_{X2}^3 x l_{X2} d - 2 x 2_{X1, X2} x l_{X1} x l_{X1} x 2_{X2} x l_{X1} x l_{X2}^2 x l_{X2}^2 B \\ &+ x l_{X1, X2} x l_{X2}^3 x 2_{X1}^3 B + x 2_{X2, X2} x l_{X1} x l_{X2}^2 B \\ &+ x l_{X1, X2} x l_{X2}^3 x 2_{X1}^3 B + x 2_{X2, X2} x l_{X1}^2 x 2_{X1}^2 B \\ &+ x l_{X1, X2} x l_{X1}^3 x 2_{X2}^3 B + x 2_{X1, X1} x l_{X2}^2 x 2_{X1}^2 A \\ &+ x 2_{X1, X1} x l_{X1}^2 x 2_{X2}^2 A + x 2_{X2, X2} x l_{X2}^2 x 2_{X1}^2 A \\ &+ x 2_{X1, X1} x l_{X1}^2 x 2_{X2}^2 A + x$$

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Symmetries of Differential Equations

Consider a general DE system

$$R^{\sigma}[u] = R^{\sigma}(x, u, \partial u, \dots, \partial^{k}u) = 0, \quad \sigma = 1, \dots, N$$

with variables $x = (x^1, ..., x^n), u = u(x) = (u^1, ..., u^m).$

Definition

A transformation

$$\begin{aligned} x^* &= f(x, u; a) = x + a\xi(x, u) + O(a^2), \\ u^* &= g(x, u; a) = u + a\eta(x, u) + O(a^2). \end{aligned}$$

depending on a parameter *a* is a *point symmetry* of $R^{\sigma}[u]$ if the equations are the same in new variables x^*, u^* .

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Example 1: translations

The translation

$$x^* = x + C, \quad t^* = t, \quad u^* = u$$

leaves KdV invariant:

$$u_t + uu_x + u_{xxx} = 0 = u_{t^*}^* + u^* u_{x^*}^* + u_{x^*x^*x^*}^*.$$

Symmetries of Differential Equations

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depending on a parameter *a* is a *point symmetry* of $R^{\sigma}[u]$ if the equations are the same in new variables x^*, u^* .

Example 2: scaling

Same for the scaling:

$$x^* = \alpha x$$
, $t^* = \alpha^3 t$, $u^* = \alpha u$.

One has

$$u_t + uu_x + u_{xxx} = 0 = u_{t^*}^* + u^* u_{x^*}^* + u_{x^*x^*x^*}^*.$$

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Nonlinear DEs

- Numerical solutions: resource/time consuming; lack generality.
- Solution methods for linear DEs do not work.
- Symmetry analysis: a general systematic framework leading to useful results.

Symmetries for ODEs

- Reduction of order / complete integration.
- All known methods of solution of specific classes of ODEs follow from symmetries!

Symmetries for PDEs

- Exact symmetry-invariant (e.g., self-similar) solutions.
- Transformations: solutions \Rightarrow new solutions.
- Mappings relating classes of equations; linearizations.
- Symmetry-preserving numerical methods.

Computation of Symmetries

- Lie point symmetries and other types are computed systematically for any DE.
- Literature widely available.
- Symbolic software packages available.
- A popular approach to analyze complicated DEs arising in applied science:
 - fluid and solid mechanics,
 - rocket science,
 - meteorology,
 - biological applications, ...

Table 1: Point symmetry classification for the 2D Ciarlet-Mooney-Rivlin models with zero forcing and $\rho_0 = \text{const} > 0$.

Case	Point symmetries
General	$Y_1 = \frac{\partial}{\partial t}, Y_2 = \frac{\partial}{\partial X^1}, Y_3 = \frac{\partial}{\partial X^2}, Y_4 = \frac{\partial}{\partial x^1}, Y_5 = \frac{\partial}{\partial x^2}, Y_6 = t \frac{\partial}{\partial x^1}, Y_7 = t \frac{\partial}{\partial x^2},$
	$\mathbf{Y}_8 = X^2 \frac{\partial}{\partial X^1} - X^1 \frac{\partial}{\partial X^2}, \\ \mathbf{Y}_9 = x^2 \frac{\partial}{\partial x^1} - x^1 \frac{\partial}{\partial x^2},$
	$Y_{10} = t\frac{\partial}{\partial t} + X^{1}\frac{\partial}{\partial x^{1}} + X^{2}\frac{\partial}{\partial x^{2}} + x^{1}\frac{\partial}{\partial x^{1}} + x^{2}\frac{\partial}{\partial x^{2}}$
A = 0,	$Y_1, Y_2, Y_3, Y_4, Y_5, Y_6, Y_7, Y_8, Y_9, Y_{10},$
B , d arbitrary	$\mathbf{Y}_{11} = f_1(X^2) \frac{\partial}{\partial X^1}, \\ \mathbf{Y}_{12} = \left(\frac{\partial}{\partial X_2} f_2(X^1, X^2)\right) \frac{\partial}{\partial X^1} - \left(\frac{\partial}{\partial X_1} f_2(X^1, X^2)\right) \frac{\partial}{\partial X^2},$
	$f_1(X^2), f_2(X^1, X^2)$ are arbitrary functions
A = d = 0	$Y_1, Y_2, Y_3, Y_4, Y_5, Y_6, Y_7, Y_8, Y_9, Y_{10}, Y_{11}, Y_{12},$
B arbitrary	$Y_{13} = t \frac{\partial}{\partial t} + X^1 \frac{\partial}{\partial X^{\mathrm{I}}}$
A = B = 0	$Y_1, Y_2, Y_3, Y_4, Y_5, Y_6, Y_7, Y_8, Y_9, Y_{10}, Y_{11}, Y_{12},$
<mark>d</mark> arbitrary	$Y_{14} = X^1 \frac{\partial}{\partial X^1}$

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Traveling Wave Ansatz

- No forcing: $R^1 = R^2 = 0$.
- Ansatz:

$$x^{i}(X^{1}, X^{2}, t) = w^{i}(z, X^{2}), \quad z = X^{1} - st, \quad i = 1, 2,$$

 $\rho_{0} = \rho_{0}(X^{2}).$

• s is the constant wave speed.

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Symmetry Classification in Traveling Wave Coordinates

#	Case	Point symmetries
1	General	$Y_1 = \frac{\partial}{\partial z}, Y_2 = \frac{\partial}{\partial w^1}, Y_3 = \frac{\partial}{\partial w^2}, Y_4 = w^2 \frac{\partial}{\partial w^1} - w^1 \frac{\partial}{\partial w^2}$
2	$ \rho_0(X^2) = (X^2 + q_1)^{q_2}, \ q_1, q_2 = \text{const}, $	$Y_1, Y_2, Y_3, Y_4,$
	$q_2 eq 0$, A, B, d, s arbitrary	$Y_5 = z \frac{\partial}{\partial z} + (X^2 + q_1) \frac{\partial}{\partial X^2} + w^1 \frac{\partial}{\partial w^1} + w^2 \frac{\partial}{\partial w^2}$
3a	$ ho_0(X^2) = \exp(q_1X^2), \ q_1 = \operatorname{const} eq 0,$	$Y_1, Y_2, Y_3, Y_4,$
	A, B, d, s arbitrary	$Y_6 = \frac{\partial}{\partial X^2}$
3b	$ \rho_0(X^2) = \exp(q_1 X^2), \ q_1 = \operatorname{const} \neq 0, $	$\mathbf{Y}_1, \mathbf{Y}_2, \mathbf{Y}_3, \mathbf{Y}_4,$
	A, d arbitrary, $B = 0, s^2 = A$	$\mathrm{Y}_{(1)}^{\infty} = -\left(rac{1}{q_1}rac{d}{dz}f_1(z) ight)rac{\partial}{\partial X^2} + f_1(z)rac{\partial}{\partial z}$
4a	$ ho_0(X^2)>0$ arbitrary,	$Y_1, Y_2, Y_3, Y_4,$
	A, B arbitrary, $d = 0, s^2 = A$	$Y_7 = z \frac{\partial}{\partial z} + w^1 \frac{\partial}{\partial w^1} + w^2 \frac{\partial}{\partial w^2}, Y_8 = \left(\rho_0 \int \frac{1}{\rho_0} dX^2\right) \frac{\partial}{\partial X^2},$
		$Y_{(2)}^{\infty} = f_2(z)\rho_0 \frac{\partial}{\partial x^2}$, $f_2(z)$ is an arbitrary function
4b	$ ho_0(X^2) > 0$ arbitrary,	$\mathbf{Y}_1, \mathbf{Y}_2, \mathbf{Y}_3, \mathbf{Y}_4,$
	A, d arbitrary, $B = 0, s^2 = A$	$Y_9 = z \frac{\partial}{\partial z}$
5a	$ \rho_0 = \text{const} $	$Y_1, Y_2, Y_3, Y_4, Y_5(q_1 = 0), Y_6,$
	A, B, d, s arbitrary	$Y_{10} = X^2 \frac{\partial}{\partial z} - \frac{Az}{A - s^2} \frac{\partial}{\partial X^2}$
5b	$ \rho_0 = \text{const}, \boldsymbol{s}^2 = \boldsymbol{A}, $	$Y_1, Y_2, Y_3, Y_4, Y_5(q_1 = 0),$
	A, B, d arbitrary	$\mathrm{Y}^{\infty}_{(3)}=f_3(z)rac{\partial}{\partial X^2}$, $f_3(z)$ is an arbitrary function
5c	$ \rho_0 = \text{const}, \ \mathbf{s}^2 = \mathbf{A}, $	$Y_1, Y_2, Y_3, Y_4, Y_5(q_1 = 0), Y_9, Y_{(3)}^{\infty},$
	A, d arbitrary, $B = 0$	シックシー 山 ・ 山 マ ・ 山 マ ・ 白 マ ・ 白 マ ・ 白 マ ・ 白 マ

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Example:

- Case: $\rho_0 = \text{const}, \quad R^1 = R^2 = 0, \quad A = s^2, \quad d = s^2 + B.$
- A basic solution:

$$w^1 = z \quad \Leftrightarrow \quad x^1(X^1, X^2, t) = X^1 - st, \qquad w^2 = x^2(X^1, X^2, t) = X^2,$$

• A symmetry-transformed solution:

$$\begin{aligned} w^1 &= z \qquad \Leftrightarrow \quad x^1(X^1, X^2, t) = X^1 - st, \\ w^2 &= X^2 - f(z) \quad \Leftrightarrow \quad x^2(X^1, X^2, t) = X^2 - f(X^1 - st) \end{aligned}$$

• Figure:

- (a) A rectangular grid in the reference configuration.
- (b) The propagating deformation, $f(z) = -\exp(-z^2)$.
- (c) The propagating deformation, $f(z) = -(1 + \tanh z)/2$.

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Examples of Exact Solutions



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Outline



- Notation; Material Picture
- Governing Equations for Hyperelastic Materials
- Constitutive Relations

2 Ciarlet-Mooney-Rivlin Solids in Two Dimensions

- Details of the Model
- Reduction of Number of Parameters

O-M-R Elasticity Equations in 2D

O Symmetry Analysis

- Symmetries of Differential Equations
- Applications of Symmetries
- General 2D Case
- Traveling Wave Coordinates
- Examples of Exact Solutions

Conclusions and Open Problems

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Conclusions

- Symmetry properties of dynamic equations for 2D planar Ciarlet-Mooney-Rivlin materials were studied:
 - in a general setting;
 - in traveling wave coordinates.
- The number of essential constitutive parameters in the model were reduced through equivalence transformations.
- New traveling-wave type exact solutions were obtained for the nonlinear model.

Future/ongoing work

- Use computed symmetries to derive new exact solutions in 2D.
- Consider important *non-planar* two-dimensional reductions (including axial symmetry), and 3D.
- Generalize to other constitutive models, in particular, models of anisotropic materials.

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Thank you for attention!

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